

**RADIATION RESPONSE AND RELIABILITY OF AlGa<sub>N</sub>/Ga<sub>N</sub>  
HEMTS**

By

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# TABLE OF CONTENTS

	PAGE
ACKNOWLEDGEMENTS .....	II
LIST OF FIGURES.....	VI
LIST OF TABLES.....	IX
<b>Chapters</b>	
ABSTRACT.....	1
CHAPTER I: INTRODUCTION .....	2
OVERVIEW OF GAN HEMTs .....	2
GROWTH TECHNIQUES OF GAN HEMTs.....	4
BRIEF INTRODUCTION OF RADIATION-INDUCED DEGRADATION .....	7
OVERVIEW OF THESIS .....	8
CHAPTER II:BACKGROUND.....	10
RADIATION DAMAGE OF GAN-BASED DEVICES.....	10
LOW FREQUENCY 1/F NOISE.....	16
CHAPTER III:DEVICE INFORMATION AND EXPERIMENT SETTINGS OF GAN HEMTs .....	19
INTRODUCTION.....	19
DEVICE INFORMATION.....	19
DC CHARACTERISTICS .....	20

TEMPERATURE DEPENDENCE .....	22
EXPERIMENT SETUP AND MEASUREMENT TECHNIQUES .....	24
CHAPTER IV: RADIATION EFFECTS OF ALGAN/GAN HEMTS .....	27
INTRODUCTION .....	27
DC MEASUREMENT AFTER X-RAY IRRADIATION .....	27
DC MEASUREMENT AFTER PROTON IRRADIATION .....	30
CONCLUSIONS .....	33
CHAPTER V: LOW FREQUENCY 1/F NOISE MEASUREMENT .....	34
INTRODUCTION .....	34
GATE BIAS DEPENDENCE OF SVD .....	34
NOISE SPECTRUM OF ALGAN/GAN HEMTS .....	38
CONCLUSIONS .....	43
CHAPTER VI: HOT CARRIER EFFECTS ON ALGAN/GAN HEMTS .....	45
INTRODUCTION .....	45
EXPERIMENT SETTINGS .....	45
DC MEASUREMENTS AND NOISE SPECTRUM ANALYSIS .....	46
CONCLUSIONS .....	48
CHAPTER VII: SUMMARY AND CONCLUSIONS .....	49
REFERENCES .....	51

## LIST OF FIGURES

	PAGE
FIG. 1-1 TYPICAL STRUCTURE OF ALGAN/GAN HEMTS.....	6
FIG. 2-1 CREATION OF AN ELECTRON-HOLE PAIR BY IONIZATION IN A SEMICONDUCTOR INSULATOR.....	11
FIG. 2-2 PLOT OF EFFECTIVE DAMAGE FACTOR VS. ELECTRON ENERGY FOR GAN SHOWING THE THRESHOLD ENERGY. ....	12
FIG. 2-3 TRANSCONDUCTANCE AND SATURATION CURRENT OF THE HEMT VS. ANNEALING TEMPERATURE.....	13
FIG. 2-4 (A) TRANSFER CHARACTERISTICS AND (B) THRESHOLD VOLTAGE SHIFT FOR ALGAN/GAN HEMTS BEFORE AND AFTER 1.8-MEV PROTON IRRADIATION AT DIFFERENT FLUENCES. ....	14
FIG. 2-5 FORMATION ENERGY OF N VACANCIES AS A FUNCTION OF THE POSITION OF THE FERMI LEVEL IN THE BAND GAP OF ALGAN.....	16
FIG. 2-6 NOISE VS. TEMPERATURE FOR N-RICH AND GA-RICH MBE AND MOCVD-GROWN DEVICES.....	18
FIG. 3-1 (A) SCHEMATIC CROSS-SECTION (B) TOPVIEW FROM MICROSCOPE OF A GAN/ALGAN HEMT.....	20
FIG. 3-4 10-KEV ARACOR 4100 X-RAY IRRADIATOR. PROBES ARE USED ON	

WAFER-LEVEL SAMPLES.....	25
FIG. 3-5 SCHEMATIC DIAGRAM OF 1/F NOISE MEASUREMENT CIRCUIT .....	26
FIG. 4-1 (A) ID-VG AND (B) CHARACTERISTICS AFTER 10-KEV X-RAY IRRADIATION .....	29
FIG. 4-2 ID-VG CHARACTERISTICS AFTER HOURS OF STRESSING WITHOUT IRRADIATION .....	29
FIG. 4-3 (A) IG-VG AND (B) ID-VG CHARACTERISTICS AFTER 1.8 MEV PROTON IRRADIATION .....	31
FIG. 4-4 THRESHOLD VOLTAGE SHIFT AS A FUNCTION OF 1.8 MEV PROTON FLUENCES	32
FIG. 4-5 TRANSCONDUCTANCE DECREASES AFTER A PROTON FLUENCE OF $1E14$ .....	33
FIG. 5-1 CROSS-SECTION OF A GAN HEMT .....	35
FIG. 5-2 (A) GATE VOLTAGE DEPENDENCE OF EXCESS DRAIN VOLTAGE LOW FREQUENCY NOISE IN ALGAN/GAN HEMTS, AT ROOM TEMPERATURE, (B) GATE VOLTAGE DEPENDENCE AT DIFFERENT TEMPERATURES .....	36
FIG. 5-3 NOISE VS. FREQUENCY BEFORE AND AFTER PROTON IRRADIATION AT DIFFERENT TEMPERATURES: (A) 300K, (B) 100K AND (C) 400K.....	39
FIG. 5-4 FREQUENCY EXPONENT OF NOISE POWER SPECTRAL DENSITY AS A FUNCTION OF TEMPERATURE .....	40
FIG. 5-5 THE NOISE SPECTRUM POWER DENSITY .....	42
FIG. 5-6 (A) ENERGY BARRIERS AND DEFECT CONFIGURATIONS (I) AND (II) OF ON-H	

(SMALLER LIGHT ATOM) AND (B) ON CONFIGURATION .....43

FIG. 6-1 THRESHOLD VOLTAGE SHIFT AS A FUNCTION OF TIME.....46

FIG. 6-2 NORMALIZED PEAK TRANSCONDUCTANCE DEGRADATION AS A FUNCTION OF  
TIME .....47

FIG. 6-3 NOISE SPECTRUM BEFORE AND AFTER HOT CARRIER STRESS .....48



## LIST OF TABLES

	Page
TABLE 1.1 THE MATERIALS PROPERTIES OF GAN COMPARED TO THE COMPETING MATERIALS.....	3
TABLE.1-2 TYPICAL VALUES OF MAXIMUM DRAIN CURRENT DENSITY AND GATE-DRAIN BREAKDOWN VOLTAGE FOR DIFFERENT HEMT TYPES .....	4
TABLE. 2-1 SRIM SIMULATION RESULTS FOR THE ALGAN/GAN HEMT DEVICES .....	15
FIG. 3-2 DC CHARACTERISTICS: (A) ID-VD, (B) ID-VG (LEFT) AND IG-VG (RIGHT) OF GAN/ALGAN HEMTS.....	22
FIG. 3-2 ID-VG AND TRANSCONDUCTANCE CURVES MEASURED AT DIFFERENT TEMPERATURE, WHEN $V_{DS} = 0.2$ V.....	24

## Abstract

Gallium Nitride (GaN)-based devices are used in space-based high power, high frequency applications due to high breakdown voltage and high carrier mobility and the large bandgap of GaN. The radiation effects and hot carrier degradation of AlGa<sub>N</sub>/GaN HEMTs are investigated in this work. Low frequency noise measurements are employed to help understand the nature of the defects that are responsible for the reliability and radiation response of GaN HEMT devices. The HEMT devices show excellent radiation hardness to 10-keV X-ray irradiation but 1.8 MeV proton irradiation results in a positive shift in the threshold voltage and reduction in current and transconductance. The temperature-dependent noise spectra show changes in defect distributions, with activation energy barriers of 0.2 eV, 0.6 eV and 0.9 eV. Density functional theory (DFT) calculations suggest that these energy levels are related to the dehydrogenation of O<sub>N</sub>-H defects. The noise spectra after hot carrier effects show similar features as those after proton exposure, strongly suggesting that dehydrogenation of O<sub>N</sub> DX centers takes place during the proton irradiation. The threshold voltage shift is negative after hot carrier stress, suggesting that other defects dominate the process that are out of the range of temperature-dependent noise measurement.

## Chapter I

### Introduction

Gallium Nitride (GaN)-based devices are used in space-based high power, high frequency applications due to their high breakdown voltage and high carrier mobility and the large bandgap of GaN.[1][2] As one of the most promising devices, GaN high electron mobility transistors (HEMTs) were observed to be extremely radiation tolerant and the radiation response and reliability of AlGaN/GaN HEMTs have been the subject of intense research for years. In this work, we study the radiation effects and hot carrier degradation of AlGaN/GaN HEMTs which are fabricated by plasma-assisted molecular beam epitaxy (PAMBE). The devices are subjected to radiation exposure or hot carrier stress and then characterized electrically. We employ low-frequency  $1/f$  noise measurements and density functional calculations to help understand the nature of defects that determine the degradation of GaN HEMT devices.

#### *Overview of GaN HEMTs*

In the past years, HEMTs based on III-V semiconductors GaAs and InP have gained a lot of success in RF applications. In 1993, the first GaN HEMT was introduced. [3] Based on wide bandgap material, GaN HEMTs have attracted lots of interest and are very promising

for high frequency, high power applications.

Table 1.1 lists the material properties of GaN compared to other competing materials. Due to a large breakdown electric field of 2 MV/cm [7], GaN devices can be easily applied into commercial systems without stepping down the operating voltage, which reduces the cost of voltage conversion. Thanks to the strong chemical bonds in the semiconductor crystal, GaN HEMTs and other GaN-based devices are also desirable for operations under high temperature and radiation exposure.

Table 1.1 The materials properties of GaN compared to the competing materials.

<b>Material</b>	$\mu$ (cm <sup>2</sup> /Vs)	$\epsilon$	$E_g$ (eV)	$T_{max}$ (°C)
Si	1300	11.4	1.1	300
GaAs	5000	13.1	1.4	300
SiC	260	9.7	2.9	600
GaN	1500	9.5	3.4	700

The heterojunction under the gate and the two-dimensional electron gas (2DEG) play a very important role in the operation of HEMTs. The 2DEG is formed when the conduction band of the barrier layer is higher than the conduction band of the channel layer. A high 2DEG sheet density is essential in HEMT design. In traditional GaAs- and InP-based HEMTs,

the barrier layer is n-doped and the donors are the sources of the 2DEG electrons. In GaN HEMTs, spontaneous and piezoelectric polarization contribute to a large interface sheet charge at the heterojunction. Both AlGaN and GaN have strong spontaneous polarization, with larger polarization in AlGaN than that in GaN. [4] Since the lattice constant of bulk AlGaN is smaller than that of GaN, the AlGaN layer is then under tensile strain, which brings in another polarization component, known as piezoelectric polarization. Due to the effects of polarization, a 2DEG with high sheet density can be achieved at the AlGaN/GaN heterojunction without intentional doping, which is a unique feature of GaN HEMTs.[1][5]

Though GaN HEMTs are updating the records of  $f_T$  and  $f_{max}$  every year, the frequency limitations are lower than that of other III-V HEMTs, especially InP HEMTs.[6][8][9] Therefore, the main prospective application and the highlight feature of GaN is high power applications, due to its large  $V_{BD}$  and high maximum drain current. High power density means that the device size can be significantly reduced and impedance matching becomes much easier.

Table.1-2 Typical values of maximum drain current density and gate-drain breakdown voltage for different HEMT types (after [6] )

<b>HEMT type</b>	<b><math>I_{max}</math> (A/mm)</b>	<b><math>V_{BD}</math> (V)</b>
GaAs HEMT	0.2~0.65	10~30
GaAs pHEMT	0.5~0.8	10~20
InP HEMT	0.6~1	3~10
AlGaN HEMT	>1	60~200

### ***Growth Techniques of GaN HEMTs***

Fig. 1-1 shows the typical structure of AlGaIn/GaN HEMTs. GaN HEMTs are commonly fabricated on either SiC or sapphire substrates due to the absence of GaN substrates. SiC has better thermal conductivity than that of sapphire and other candidate materials like AlN, Si and complex oxides. Concerning self-heating, SiC substrates are preferable. But sapphire is still being widely used because of less cost compared to SiC. GaN HEMTs on Si substrates have been also been reported. Si substrates receive lots of interest not only because of low cost, but also due to good thermal conductivity (about three times larger than that of sapphire).[10] These typical substrate materials remediate the lattice mismatch when single crystal GaN is still unavailable. However, since the efficiency of high power devices is highly dependent on operating frequency and temperature, cooling is quite important to maintain high electrical performance and reliability.[11] To remediate the junction temperature, diamond substrates have been heavily investigated.[12][13][14] GaN-on-diamond demonstrated half the thermal resistance of GaN-on-SiC, yet the output power of GaN-on-diamond devices is limited by the relatively lower current density. [15]

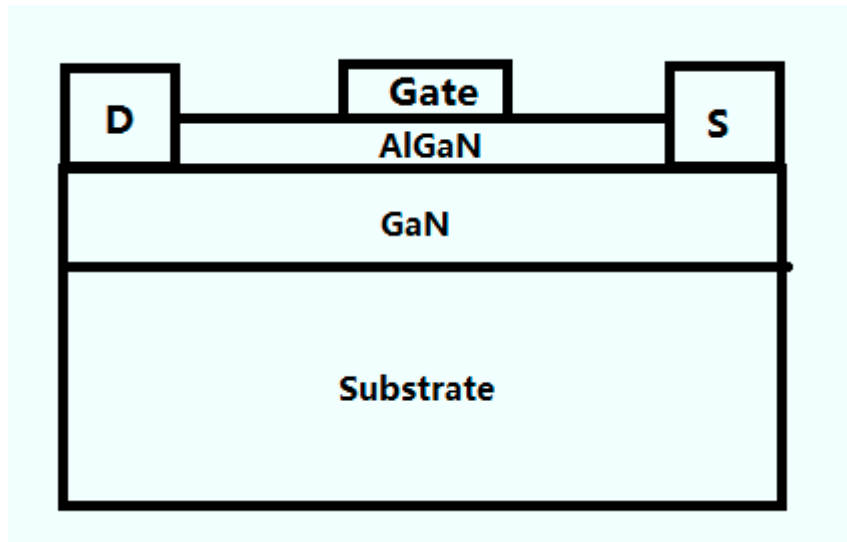


Fig. 1-1 Typical structure of AlGaIn/GaN HEMTs

The AlGaIn and GaN layers can be either grown by molecular-beam-epitaxy (MBE) or metal-organic chemical vapor deposition (MOCVD) on sapphire, SiC, or Si substrates. The MBE technique offers growth at lower temperatures (550 °C to 880 °C, compared to MOCVD, which is higher than 1000 °C) and can achieve precise interfaces, which improves transport properties. The MBE research has divided itself into two different camps by using nitrogen plasma sources and ammonia sources, respectively. These two techniques have their own advantages and a combination of the two can potentially provide new opportunities. Ga-rich plasma-assisted MBE (PAMBE) can achieve flat surfaces at lower temperatures but it usually needs to grow on high quality GaN templates made by MOCVD to obtain best results, while NH<sub>3</sub>-MBE readily obtains high electron mobility GaN layers on SiC or sapphire substrates with larger surface roughness. [16]

The nucleation layer of GaN or AlN is deposited at a low temperature (typically 600 °C to 900 °C) on SiC or sapphire substrates. [1][17] As the growth of GaN structure requires careful matching of the GaN lattice to the substrate, the nucleation layer affects the electrical

properties of the HEMT structures significantly.

### **Brief Introduction of Radiation-induced Degradation**

The radiation hardness of GaN-based devices exposed to energetic particles that produce displacement damage is about one order of magnitude higher than for competitors like AlGaAs/GaAs HEMTs, as a consequence of higher binding energy in GaN. A higher binding energy translates to a reduced introduction rate of primary radiation defects. The energetic particles in space causing permanent damage in electronics include protons, electrons and heavy charged particles. A variety of effects in the characteristics of GaN HEMTs system can occur after radiation exposure:

- (1) Shift in pinch-off voltage
- (2) Increase in junction leakage
- (3) Mobility degradation
- (4) Increase in noise

Several different physical processes are involved when these energetic particles interact with semiconductor devices. The first process is ionization, when charged particles interact with target materials and create electron-hole pairs in it. The second process is displacement damage when an incident particle transfers enough energy to move the target atom from its normal lattice position to another position, creating a vacancy in the lattice.

MOS transistors and other semiconductor devices sensitive to charge trapping are strongly affected by ionization damage, changing key properties like gate threshold voltage



and leakage current. Due to higher surface state density in GaN, ionization effects are less important compared to silicon-based devices. Moreover, the insertion of buffer or capping layer isolate surface trapping from the active region of the devices. Therefore, most research shows that displacement damage is more dominant than ionization effects in AlGaIn/GaN HEMTs.

### *Overview of Thesis*

This thesis concentrates on the radiation response, mainly proton-induced degradation of GaN/AlGaIn high electron mobility transistors, and identifies the responsible defects. The techniques used in this thesis are not restricted to GaN-based systems and can be used in other semiconductor materials.

The mechanisms of radiation damage and previous works are reviewed in Chapter II. GaN-based devices exhibit excellent radiation hardness under a wide range of experimental conditions. The theory of low frequency noise measurement is also introduced briefly.

In Chapter III, the structure and DC characteristics of the AlGaIn/GaN HEMTs are introduced, along with the measurement techniques employed. All the DC characteristics in the remainder of this work are measured using the same experiment settings.

The effects of X-ray and 1.8 MeV proton irradiation are shown in Chapter IV. The devices show superior radiation tolerance to 10 keV X-ray irradiation, and degradation in DC characteristics were observed after 1.8 MeV protons. We employed the  $1/f$  noise

measurements and density functional theory (DFT) calculations to understand the nature of the defects, as discussed in Chapter V. The gate voltage dependence of noise is also shown.

Chapter VI reports the hot carrier effects of AlGaIn/GaN HEMTs. The DC characteristics and noise spectra are compared to those following of proton irradiation.

Chapter VII provides the summary and conclusions of this work.

## Chapter II

### Background

#### *Radiation Damage of GaN-based Devices*

In space environments, energetic particles incident on semiconductor devices lose their energy to ionizing and nonionizing processes as they travel through the devices. The energy loss causes the production of electron-hole pairs (ionization) and displaced atoms (displacement damage).

##### A. Ionization effects

In ionization process, energy is transferred to an electron in the valence band by the incoming particle, raising it to the conduction band and creating a corresponding hole in the valence band. This process is shown in Fig. 2-1. The minimum energy required to create electron-hole pairs is approximately the bandgap energy.

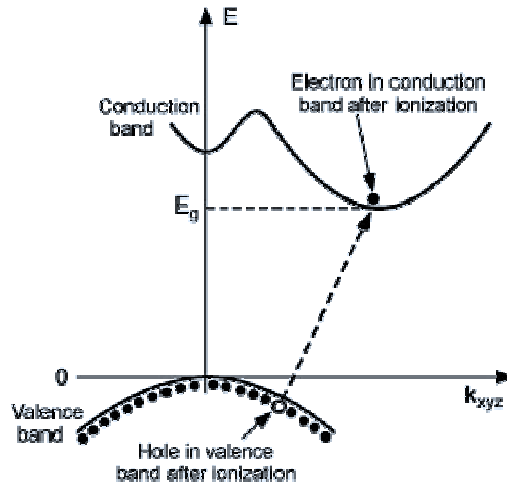


Fig. 2-1 Creation of an electron-hole pair by ionization in a semiconductor insulator. (after [18].)

Irradiation results in the generation of defects, with the defect creation rates depending on sample quality and doping level. [19][20][21] Significant degradation of AlGaN/GaN HEMTs was observed only after a  $\gamma$ -ray ( $^{60}\text{Co}$ ) dose of many tens or even hundreds of Mrad(Si). [22],[23]. Devices show a negative shift in threshold voltage, which is dominated by an increase in trap density. Other experiments [24], [25] and [26] with similar results suggest that damage due to particle irradiation is of much more concern in GaN-based devices, which are more sensitive to displacement damage than ionization effects.

### B. Displacement damage

The threshold energy for a specific material can be determined by measuring the energy dependence of displacement damage. For GaN, it is initially measured in [27], by monitoring changes as a function of electron irradiation energies in the range of 300 – 1400 keV. The formation of Ga vacancies started at an electron energy of 440

keV ( $E_{threshold}$ ), shown as the x-intercept in Fig. 2-2. The corresponding Ga displacement energy threshold was calculated as  $19 \pm 2$  eV via, [27]

$$E_{displacement,Ga} = \frac{2E_{threshold}(2m_e c^2 + E_{threshold})}{M_{Ga} c^2}. \quad (1)$$

The defect production depends on irradiating particle type and energy, considering the difference in defect self-annealing rates. In molecular dynamics calculations of displacement effects in GaN, a wide distribution of threshold energies for both Ga and N sublattices are observed. People found the minimal energies of defect formation of 18 eV for Ga and 22 eV for N, while the average displacement energies were much higher, 45 eV for Ga and 109 eV for N. [28] The average thresholds are much higher than the average recoil energies (less than 20 eV [29]), which suggests that the degradation after irradiation is hard to explain only by the displacement of atoms from a perfect lattice.

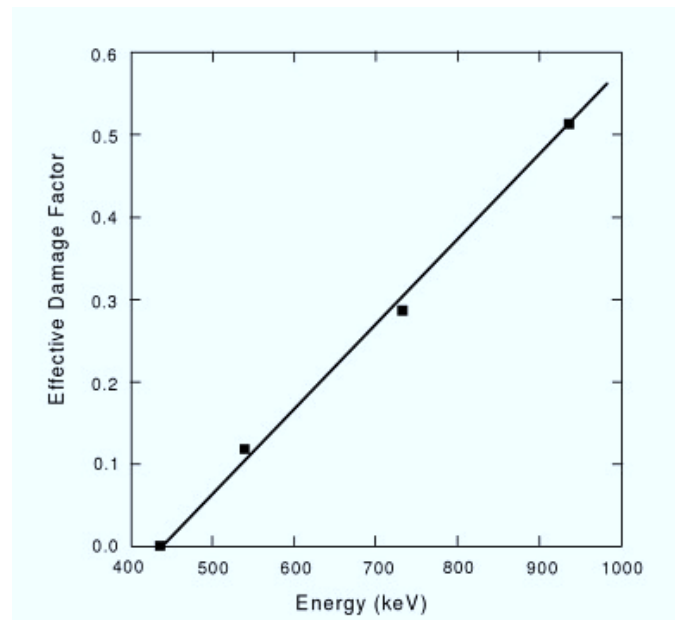


Fig. 2-2 Plot of effective damage factor vs. electron energy for GaN showing the threshold energy. (after [27] )

Most of the work has been focused on the effects of protons, neutrons, and electrons. Proton damage and annealing effects in GaN/AlGaN HEMTs were initially investigated by Cai. *et al.* [30] Figure 2-3 shows that the dc current and transconductance decreased from 260 to 100 mA/mm and from 80 to 26 mS/mm, respectively, for a 1.8 MeV proton fluence of  $10^{14}$  p+/cm<sup>2</sup>. The damage was stable at room temperature and some of the damage annealed when temperature was raised to over 600 °C. They suggested that the lattice strain may play a role in annealing at very high temperature.

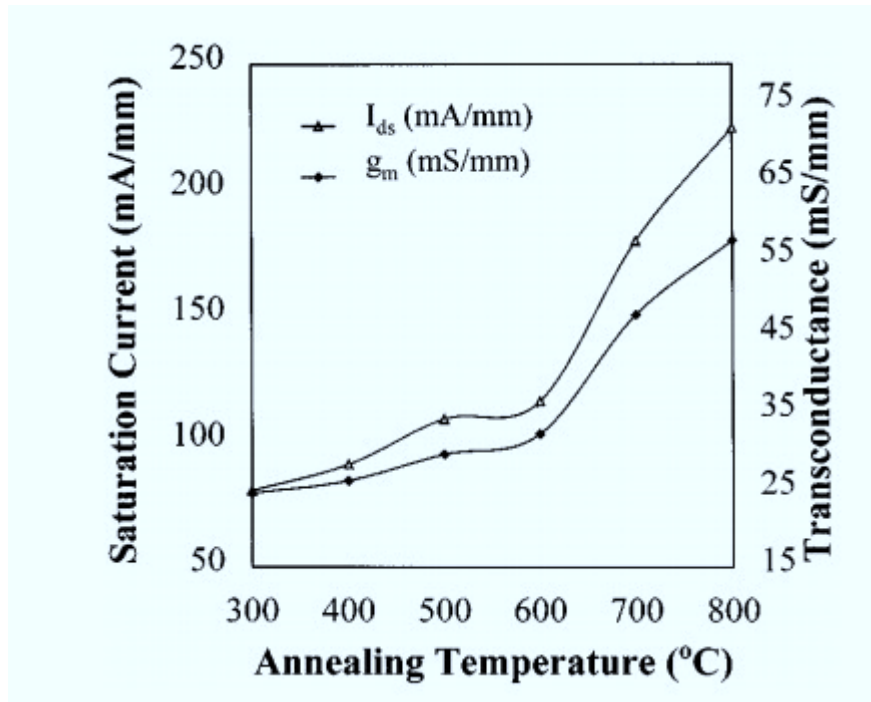
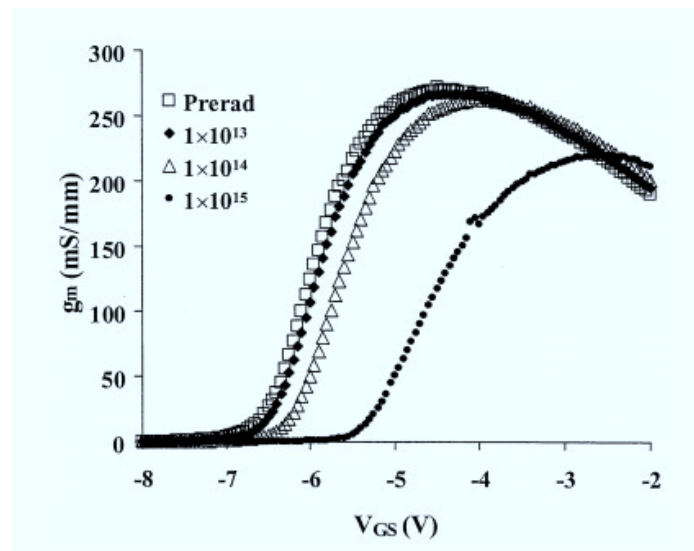


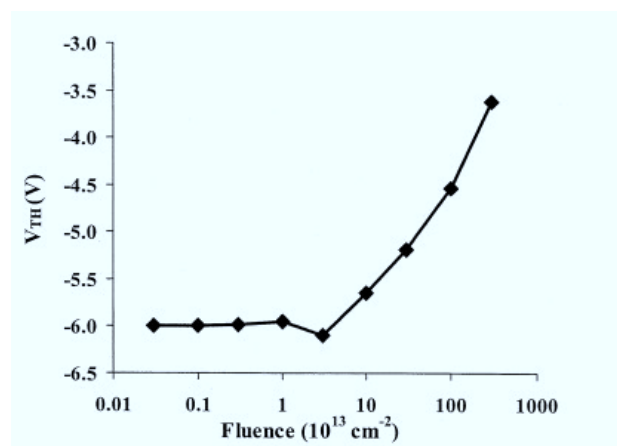
Fig. 2-3 Transconductance and saturation current of the HEMT vs. annealing temperature at  $V_{ds} = 10$  V, and  $V_g = 0.5$  V. Before irradiation,  $g_{m0} = 80$  mS/mm,  $I_{ds0} = 260$  mA/mm. (after [30])

Similar proton irradiation studies at different energies ([31] - [37]) suggest that GaN-based devices are extremely radiation hardened and proton energy has a strong effect on the amount of damage created in the 2DEG of the HEMT because of

differences in nonionizing energy loss. [38][39] Fig. 2-4 shows the transconductance degradation and threshold voltage shift after 1.8 MeV proton irradiation, performed by Hu. *et al.* [33] The devices they tested used a thin AlN layer between the AlGaIn and GaN layers which increased the sheet carrier mobility due to higher conduction band discontinuity. No significant degradation was observed at fluences up to  $10^{14}$  / $\text{cm}^2$ , which suggests excellent radiation hardness.



(a)



(b)

Fig. 2-4 (a) Transfer characteristics and (b) threshold voltage shift for AlGaIn/GaN HEMTs before and after 1.8-MeV proton irradiation at different fluences. (after [33] )

To understand the effects of radiation species in space environments, Sonia *et al.* [40] irradiated devices with 2 MeV protons, carbon, oxygen, iron, and krypton ions with fluences ranging from  $1 \times 10^9/\text{cm}^2$  to  $1 \times 10^{13}/\text{cm}^2$ . Hu *et al.* [26] conducted the energy dependence experiment of proton-induced degradation at 1.8, 15, 40, and 105 MeV. The maximum transconductance and saturation current reductions were obtained at 1.8 MeV energy and fluences of  $10^{12}/\text{cm}^2$ , due to much larger non ionizing energy loss, as shown in Table 2-1.

Table 2-1. SRIM [41] Simulation results for AlGaIn/GaN HEMT Devices. The sensitive layer thickness was 3.54  $\mu\text{m}$ . IEL: Ionizing Energy Loss; NIEL: Non-Ionizing Energy Loss (after [26])

Energy Loss	1.8 MeV	15 MeV	40 MeV	105 MeV
IEL (keV/Ion)	114	26.2	12.2	6.1
NIEL (eV/Ion)	3.1	0.27	0.1	0.05
Maximum fluence ( $\text{cm}^{-2}$ )	$10^{12}$	$5 \times 10^{10}$	$10^{11}$	$10^{13}$
Total Ionizing Dose (rad(Ga))	$1.1 \times 10^6$	$1.7 \times 10^4$	$1.6 \times 10^4$	$8.0 \times 10^5$

Roy *et al.* studied the 1.8-MeV proton radiation response of GaN HEMTs fabricated under Ga-rich, N-rich and  $\text{NH}_3$ -rich conditions. Positive shifts in pinch-off voltage were obtained in all three kinds of devices and N vacancies were suggested to be responsible for an increase in  $1/f$  noise after irradiation. [35][42] N vacancies and divacancies can be generated during the irradiation. At the operating bias condition,



these acceptor-like traps were negatively charged, leading to the positive shift in  $V_{th}$ . The dashed line in Fig. 2-5 pointed out the estimated Fermi level under the bias used for noise measurement. The slope changes from -1 to -2, indicating the charge states of defects became more negative, leading to an increase in noise after irradiation.

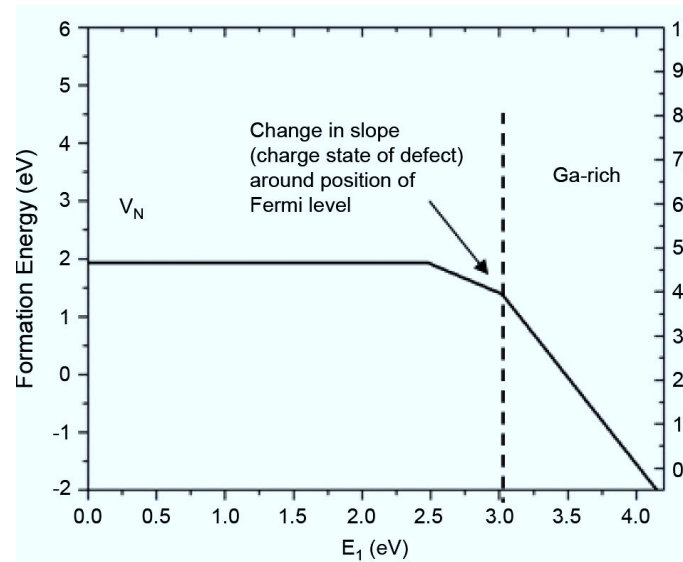


Fig. 2-5 Formation energy of N vacancies as a function of the position of the Fermi level in the band gap of AlGaN.

### Low Frequency 1/f Noise

Many physical systems exhibit spontaneous fluctuations (noise), which contains a large amount of information about a system and its interaction with the surrounding environment. When a constant bias is applied to a semiconductor device, the current will show fluctuations and the spectral density varies over a large range of frequencies. Two frequently sources of current-induced noise are observed. At high frequencies, the noise is white, and results from a combination of shot noise and Johnson noise.

However, at sufficiently low frequencies, the noise is proportional to  $1/f^\alpha$  (with typical value of  $\alpha$  close to 1). This noise is known as  $1/f$  noise, pink noise, or flicker noise.

There are a variety of mechanisms that have been considered to be responsible for noise in the intrinsic HEMT, e.g., carrier velocity fluctuation, gate leakage, and traps. [43][44] The velocity fluctuation corresponds to the thermal noise and the gate leakage noise is associated with electron injection into the channel over the gate Schottky barrier, which is frequency independent. Here we consider the effects causing by trapping of electrons in interface traps (located at AlGaIn/GaN interface), which leads to a  $1/f$  dependence. We define the excess drain-voltage noise power spectral density  $S_V$  as [45],

$$S_V = K f^{-\alpha} \frac{(V_d)^2}{(V_g - V_{th})^2} \quad (2)$$

$$K \equiv S_V f (V_g - V_{th})^2 V_d^{-2} \quad (3)$$

$K$  is the device-dependent normalized noise magnitude.  $V_g$ ,  $V_{th}$  and  $V_d$  stand for the gate voltage, the pinch-off voltage and the drain voltage, respectively.  $S_V$  is measured in the linear regime of device operation and is proportional to  $f^{-\alpha}$ , with  $\alpha$  value close to unity. [35][46][47]

Dutta and Horn [48] have shown that noise magnitude of metal films typically has a strong temperature dependence. They also demonstrated that the temperature dependence of the  $1/f$  noise could be due to a thermally activated random process with a distribution of activation energies, which is proportional to the temperature.

Previous work involving studies of the  $1/f$  noise of GaN HEMTs as a function of temperature (Fig. 2-5) has revealed significant insight into the nature and energy structure of the defects that cause the noise. [49] The noise spectra of three kinds of devices show a common peak at 0.2 eV, which is related to the O DX center. The N-rich devices show a possible peak at  $> 400$  K, where nitrogen antisite defects may be responsible.

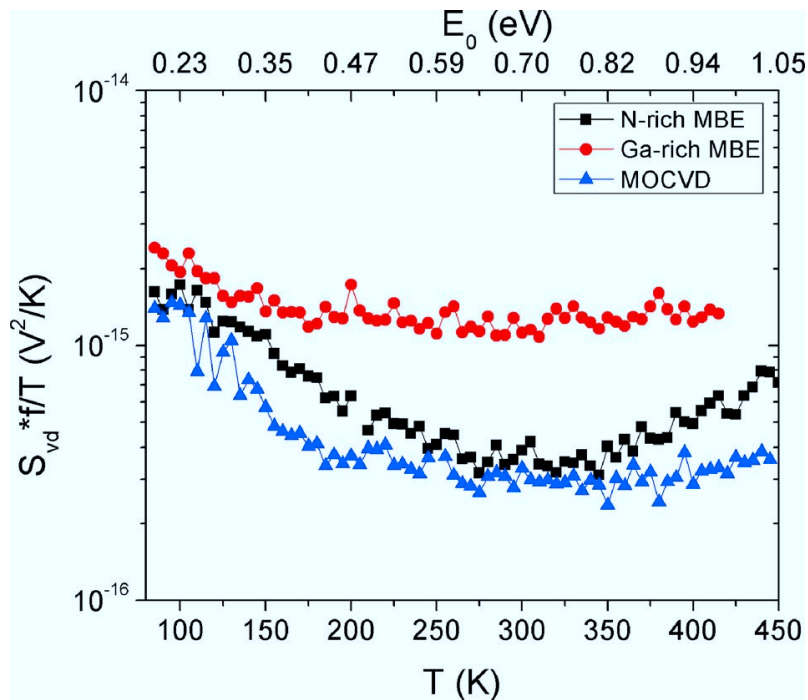


Fig. 2-6 Noise vs. temperature for N-rich and Ga-rich MBE and MOCVD-grown devices.  $f = 10$  Hz. (after [49])

In this work, the temperature dependence of AlGaN/GaN HEMTs will be described in chapter V and VI. The low frequency noise measurements are employed as a sensitive probe of impurities and defects that affect the radiation response and reliability issues for GaN HEMTs.

## Chapter III

### Device Information and Experiment Settings of GaN HEMTs

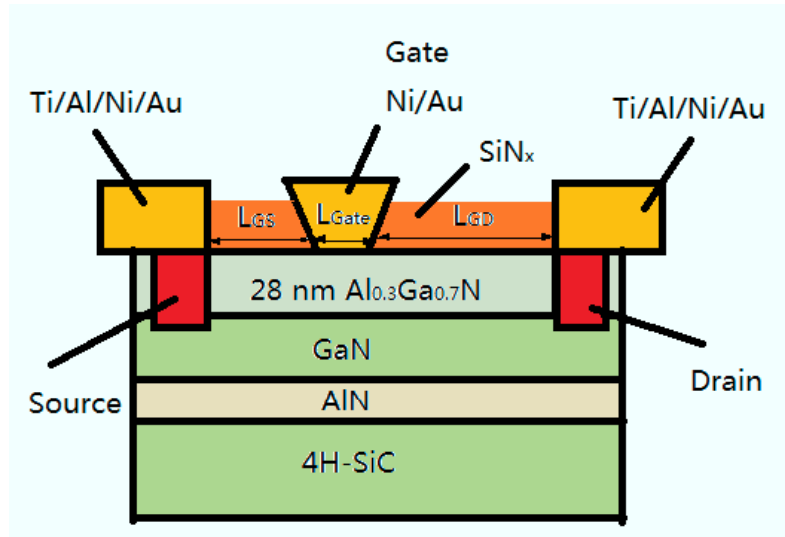
#### Introduction

This chapter describes the AlGaIn/GaN HEMTs and the DC and  $1/f$  noise measurement techniques employed here. The bias conditions and settings of radiation exposure are also introduced.

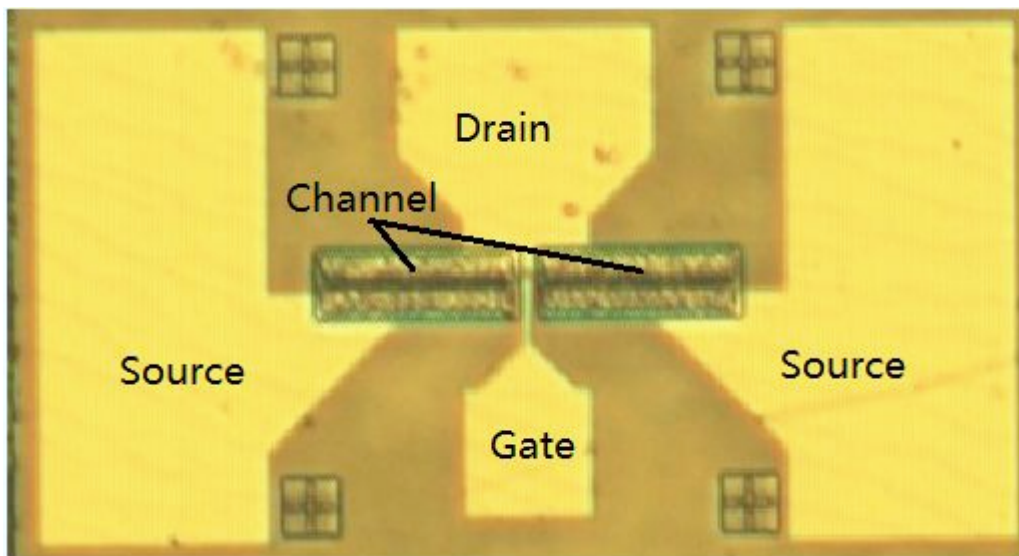
#### Device Information

AlGaIn/GaN HEMTs were fabricated on AlGaIn/GaN heterostructure layers grown by plasma-assisted molecular beam epitaxy (PAMBE) on SiC substrates at the University of California, Santa Barbara.

The schematic cross-section of a GaN HEMT is shown in Fig 3.1(a) and the top view of the device is shown in Fig 3.1(b). The MBE growth of the GaN and AlGaIn layers was performed under Ga-rich conditions, which provides lower surface roughness. [50] The devices are 150  $\mu\text{m}$  wide. The gate length of the samples is 0.7  $\mu\text{m}$ ;  $L_{GD} = 1 \mu\text{m}$  and  $L_{GS} = 0.5 \mu\text{m}$ . The 2DEG lies below the AlGaIn layer and a buffer layer of AlN separates the GaN and the SiC substrate.



(a)



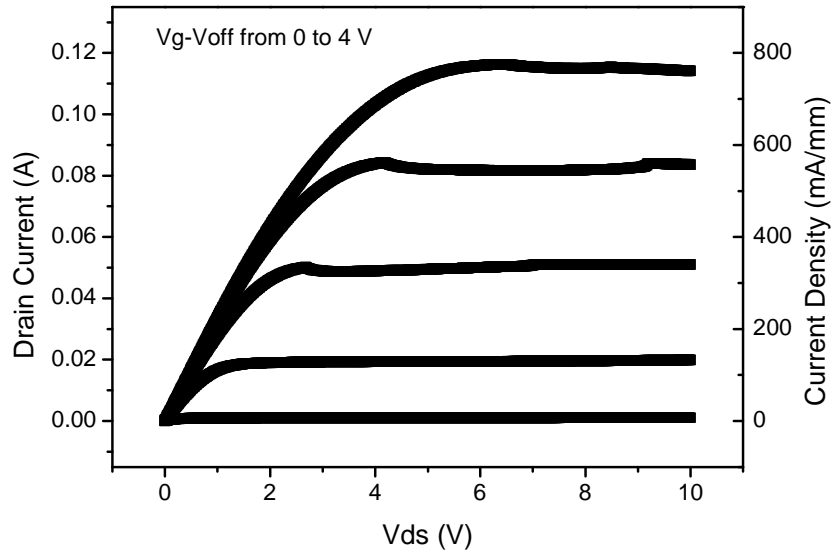
(b)

Fig. 3-1 (a) Schematic cross-section (b) topview from microscope of a GaN/AlGaN HEMT. The channel width is 75  $\mu\text{m}$  on each side of the gate.

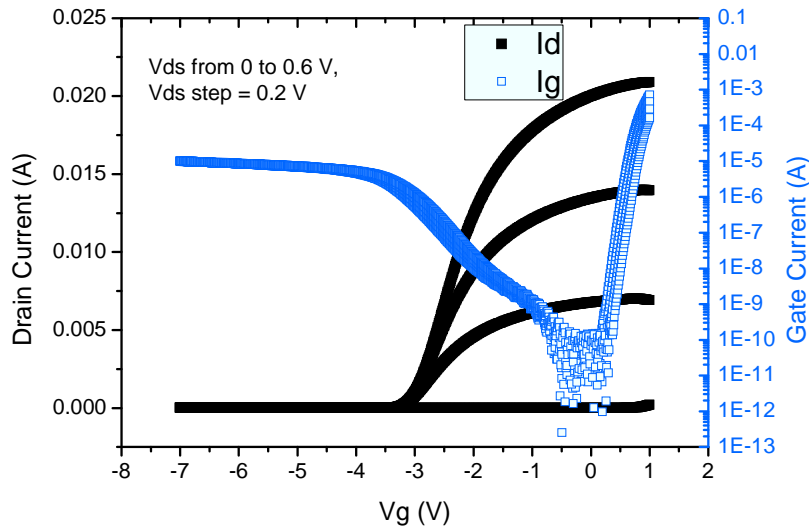
### DC Characteristics

The DC characteristics are measured with HP 4156B and Agilent B1505 parameter analyzers. Fig. 3.2 shows the DC characteristics for a typical Ga-rich

GaN/GaN HEMTs. In Fig. 3-2(a),  $I_d$ - $V_d$  curves of AlGaN/GaN HEMTs are shown.  $V_{gs}$  starts from  $V_{th}$ , with  $V_{gs}$  step = 1 V.  $V_{ds}$  swept from 0 to 10 V. The saturation current is around 120 mA at  $V_g - V_{th} = 4$  V, corresponding to a current density of 800 mA/mm. Fig. 3-2(b) (left) shows the  $I_d$ - $V_g$  characteristics, with a pinch-off voltage of -3.41 V here. For other HEMTs in this thesis, it varies from -3 to -5 V. The gate length is 0.7  $\mu\text{m}$ , corresponding to a gate leakage current density of  $\sim 2$  mA/mm around pinch-off (Fig. 3-2(b) (right)).



(a)



(b)

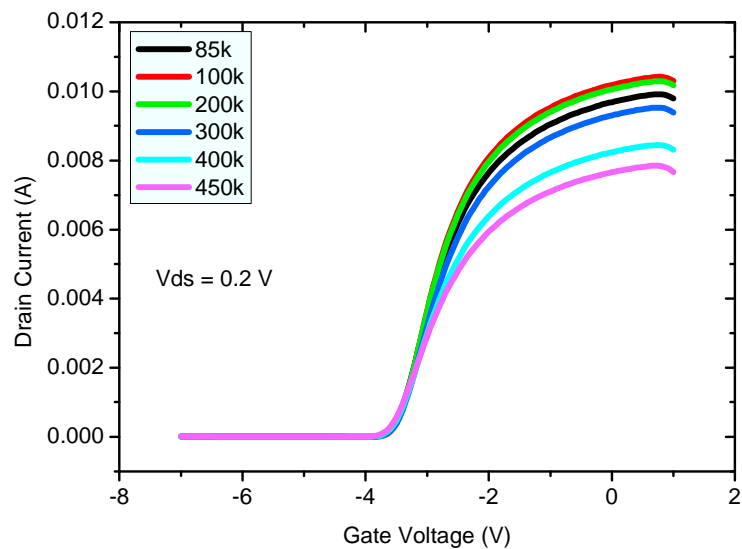
Fig. 3-2 DC characteristics: (a)  $I_d$ - $V_d$ , (b)  $I_d$ - $V_g$  (left) and  $I_g$ - $V_g$  (right) of GaN/AlGaN HEMTs.

### Temperature Dependence

The DC characteristics change with temperature. In this work, current-voltage shift are compared at a fixed temperature, usually 300 K. The temperature dependence of DC characteristics is shown in Fig. 3-3. The temperature range used in this work is from 85 K to 450 K. The threshold voltage does not change much over the whole temperature range, as shown in Fig. 3-3(a), indicating the sheet carrier density remains almost constant in this experiment. Both the on-state current and peak transconductance decrease from 200 K to 450 K, which is related to smaller electron mobility in the 2DEG due to more scattering in the channel when heating the devices. This mechanism dominates around 300 K, but at lower temperature ( $< 200$  K), it

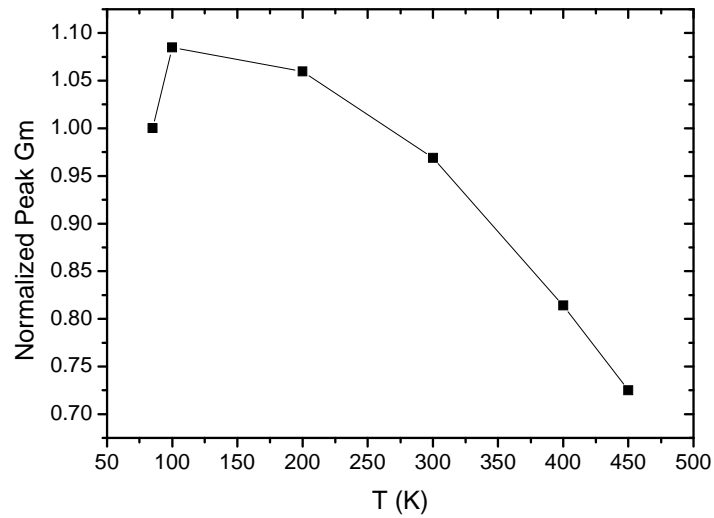
becomes negligible so that the reduction from 100 K to 200 K is quite small. However, the 85 K curve lies in the center, not the highest of the whole data set, and Fig. 3-2(b) show that the peak transconductance decreased from 100 K to 85 K. In the “freeze-out” temperature region ( $< 100$  K), the number of free carriers decreases exponentially and meanwhile, the electron mobility also goes down due to an increase in the Coulomb scattering.

As the pinch-off voltage changes with temperature, the devices are biased at a fixed voltage from the pinch-off voltage when doing the temperature-dependent noise measurement.



(a)





(b)

Fig. 3-2 (a)  $I_d$ - $V_g$  curves and (b) peak transconductance measured at different temperature, when  $V_{ds} = 0.2$  V.

### **Experiment Setup and Measurement Techniques**

#### X-ray irradiation:

Devices were irradiated at room temperature with a 10-keV ARACOR 4100 X-ray Irradiator (Fig. 3-4). Charge trapping effects usually take place in insulators. There is no oxide layer in these HEMT structures as there is in a Si based MOSFET. The gate is biased at +2 V ( the electric field near the gate edge is  $\sim 2$  MV/cm), with drain and source terminals grounded. DC characteristics are measured before and after irradiation (total dose from 500 krad( $\text{SiO}_2$ ) to 8 Mrad( $\text{SiO}_2$ )), and room temperature annealing is monitored for  $\sim 10$  hours. A control stress experiment is also performed

at the same bias condition but without irradiation.

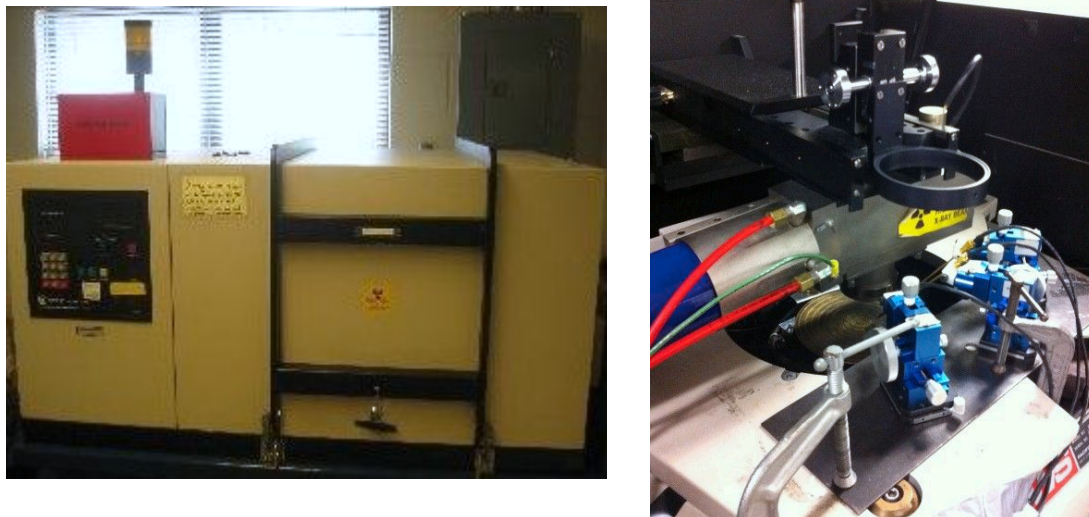


Fig. 3-4 10-keV ARACOR 4100 X-ray irradiator. Probes are used on wafer-level samples.

#### Proton irradiation:

The AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs were irradiated with 1.8 MeV protons to a fluence of  $1 \times 10^{14} \text{ cm}^{-2}$  using the Vanderbilt Pelletron facility, with all pins grounded. The proton energy is chosen for large NIEL (more than 20 times more damaging than 50-MeV protons) and  $1 \times 10^{14} \text{ cm}^{-2}$  is a very high particle fluence.[51] The irradiation is performed at room temperature. DC and  $1/f$  noise measurement are taken before and after exposure. The damage to the devices is stable as little annealing was observed under room-temperature therefore the annealing curves will not be shown in this part.

#### $1/f$ noise measurement:

Low frequency  $1/f$  noise is measured for AlGaN/GaN HEMTs, before and after radiation/stress. The excess noise measurements were performed when the devices were biased in the linear regime, supplied by a HP 4140B constant voltage supply. A resistor is connected to the drain terminal for protecting and adjusting the drain bias. The gate voltage is adjusted so that the noise originates from the gated portion of the channel. The drain voltage noise is then amplified using a low-noise amplifier SR 560 and the power spectral density was calculated by a SR 760 spectrum analyzer, across a frequency span from 6 Hz to 390 Hz.

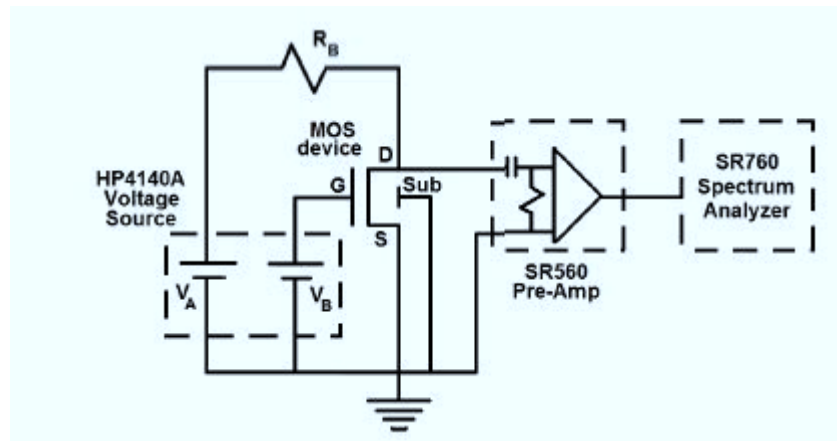


Fig. 3-5 Schematic diagram of  $1/f$  noise measurement circuit (after [53]).

## Chapter IV

### Radiation Effects on AlGaN/GaN HEMTs

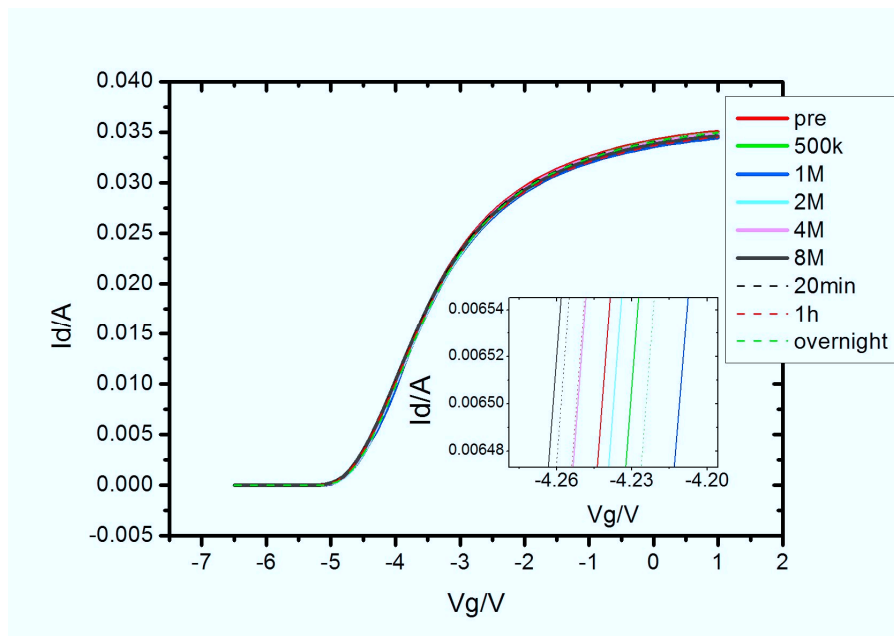
#### Introduction

Most previous studies of radiation effects of GaN HEMTs suggest significant radiation tolerance and ionizing damage is less important compared to displacement damage. Due to higher surface state density, much higher total dose levels are required to affect the interface-trap density. Moreover, in many AlGaN/GaN HEMTs, there is no oxide or other insulators at the gate or anywhere else in the structure. Therefore, no TID degradation would be expected. [52] In this work, considering the 10 nm SiN<sub>x</sub> passivation layer, the TID effects of AlGaN/GaN HEMTs were checked by irradiating with 10-keV X-rays. 1.8 MeV proton irradiation was performed later and more damage was observed.

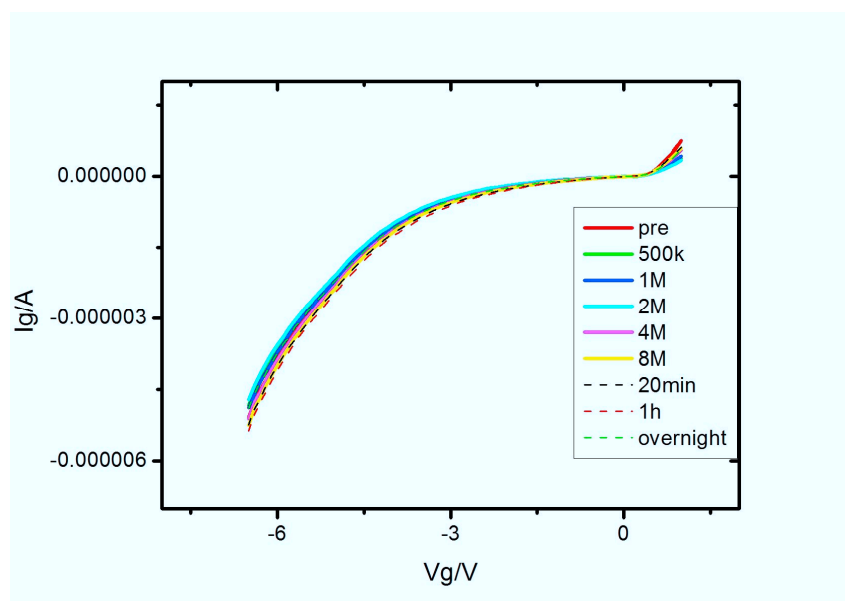
#### DC Measurement after X-ray Irradiation

The  $I_d$ - $V_g$  and  $I_g$ - $V_g$  characteristics of the HEMTs are shown in Fig. 4-1(a) and (b), respectively, before and after total doses of 500 k, 1 M, 2 M, 4 M and 8 Mrad(SiO<sub>2</sub>). The measurement is taken at  $V_{ds} = 1$  V. Curves overlap each other and the net threshold voltage shift before and after 8 Mrad(SiO<sub>2</sub>) is very tiny (a few mV),

suggesting significant radiation tolerance. From the bottom inset, which magnifies the changes from the marked area, the curves were firstly shifting positively and then moving backwards, indicating the same trend of threshold voltage. Similar observations were found in the gate leakage current, which firstly increased and later decreased.



(a)



(b)

Fig. 4-1 (a)  $I_d$ - $V_g$  and (b) characteristics after 10-keV X-ray irradiation. Very small net  $V_{th}$  shift is observed after 8 Mrad( $\text{SiO}_2$ ).

The net negative threshold voltage shift indicates the generation of trapped charge in the AlGaIn layer, though the voltage shift is very tiny. After hours of room-temperature annealing, the shift recovers, shown as the dashed curves in Fig. 4-1(a). The last annealing curve shows that the “damage” is totally recovered and the net threshold voltage shift is positive again.

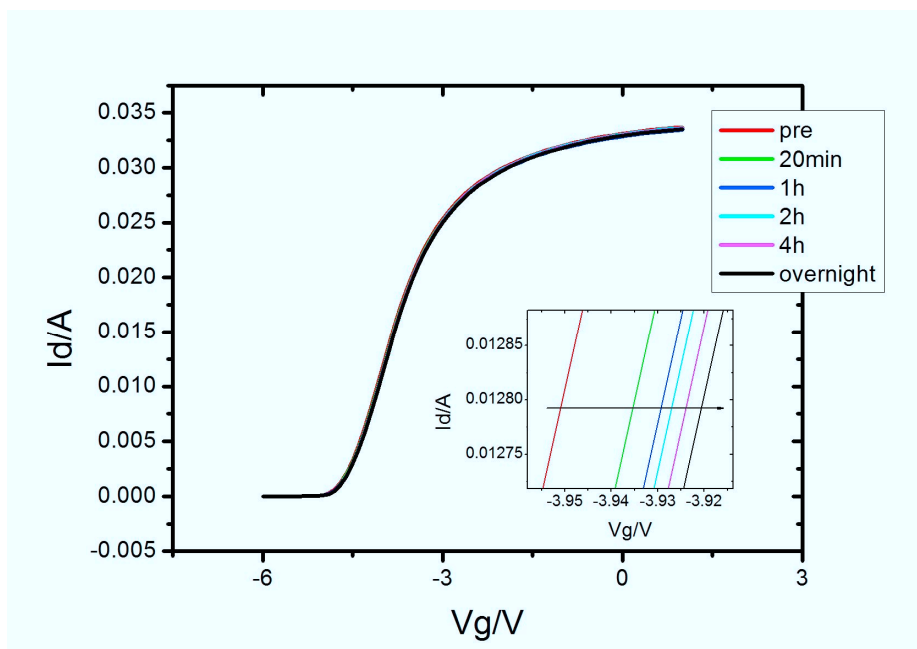


Fig. 4-2  $I_d$ - $V_g$  characteristics after hours of stressing without irradiation. The gate was biased at 2 V while other terminals were grounded.

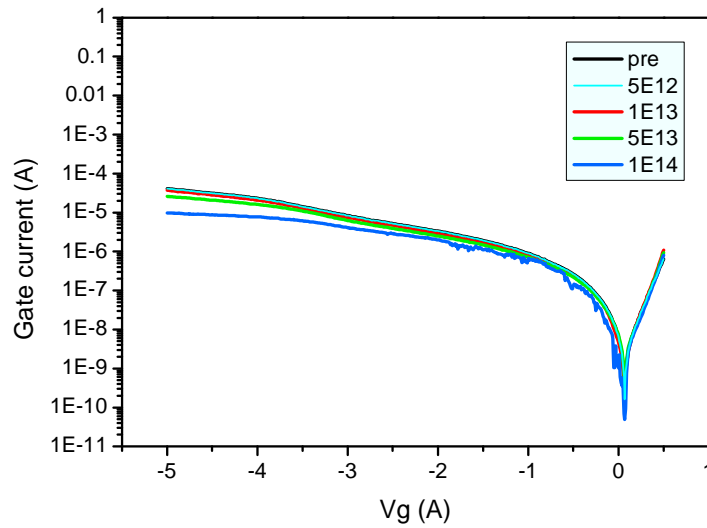
A control experiment was performed under the same bias conditions without irradiation. In this case, the  $I_d$ - $V_g$  curves moved monotonically to the positive (Fig. 4-2). The magnitude of shift is about the same level of the previous X-ray irradiation experiment. In the first 20 minutes, the curves shift rapidly, about 50% of the total net

shift and after 15 hours (black “overnight” curve), the shift reached saturation. This explains the changes in X-ray irradiation. At small doses, the shift is dominated by the stress so that it moves first positively. When total dose effects get larger, the curves move backwards and a net negative shift is observed when total dose is larger than 4 Mrad(SiO<sub>2</sub>). During the annealing, with only stressing, the curves start moving positively, monotonically. When annealing time is longer enough (before saturation), the effects of total dose is recovered and then last annealing curve (Fig. 4-1(a)) locates at the positive side of the pre-irradiation curve. Since the effects of total dose and stressing are at the same level, the  $I_d$ - $V_g$  curves overlap each other and move back-and-forth during the X-ray irradiation, in a very tiny scale (a few mV) which can be neglected.

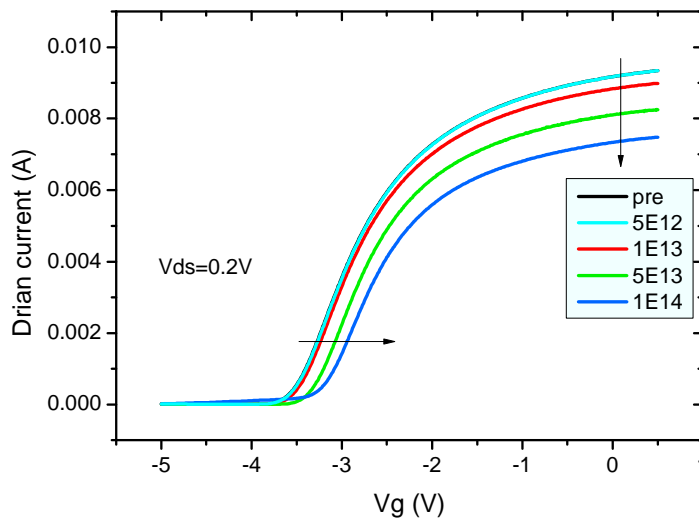
### **DC Measurement after Proton Irradiation**

Previous proton irradiation studies ([31] - [37]) suggest that GaN-based devices are extremely radiation hardened and proton energy has a strong effect on the amount of damage created in the 2DEG of the HEMT. In this work, the Ga-rich AlGa<sub>x</sub>N/GaN HEMTs were subjected to 1.8 MeV proton irradiation and the DC characteristics before and after radiation exposure were measured to help identify the nature of the defects created, shown in Fig. 4-3. Little change in forward gate current is observed after a proton fluence of  $1 \times 10^{14}$  cm<sup>-2</sup>, indicating that the Schottky barrier height of the gate contact does not degrade much during the irradiation. The reverse gate current

decreased with increasing proton fluences. From Fig. 4-3(b), a positive shift in pinch-off voltage and degradation in on-state current are observed.



(a)



(b)

Fig. 4-3 (a)  $I_g$ - $V_g$  and (b)  $I_d$ - $V_g$  characteristics after 1.8 MeV proton irradiation. The measurement is taken at  $V_{ds} = 0.2$  V.



The positive shift in pinch-off voltage with increasing fluence, shown in Fig. 4-4, indicates the creation of acceptor-like traps. Previous reports show that the defects causing the degradation are created in the AlGaN. A reduction in on-state drain current is observed, which is about 20% after the proton fluence of  $1 \times 10^{14} \text{ cm}^{-2}$ . This suggests the degradation in carrier mobility and transconductance, due to the generation of more traps.[29][34] Fig 4-5 compare the transconductance before and after proton irradiation. The peak transconductance drops 11%, showing a positive shift that is consistent with  $V_{th}$  shift due to acceptor-like traps' generation by proton bombardment. The traps are charged, and are responsible for Coulomb scattering of electrons in the channel, thus reducing the mobility and the peak transconductance.

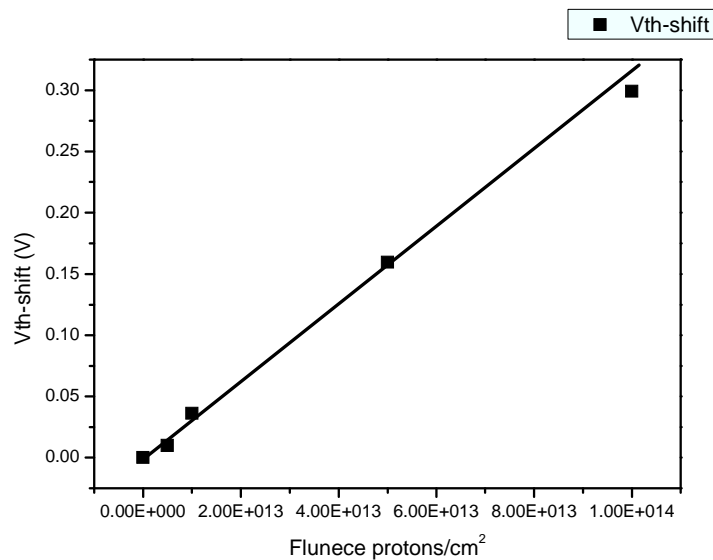


Fig. 4-4 Threshold voltage shift as a function of 1.8 MeV proton fluences.

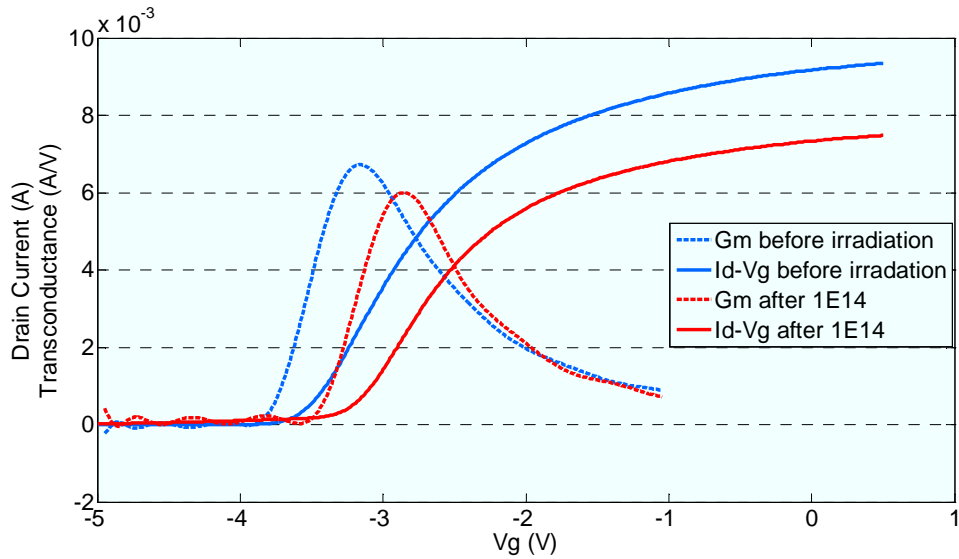


Fig. 4-5 Transconductance decreases after a proton fluence of  $10^{14}/\text{cm}^2$ .

### **Conclusions**

In this chapter, the radiation response of devices irradiated with 10 keV X-rays and 1.8 MeV protons are studied. As there is no oxide in the HEMT structure, the devices show excellent radiation tolerance to X-ray irradiation. After 1.8 MeV proton irradiation, reduction in current and transconductance, and shift in pinch-off voltage were observed. The generation of acceptor-like traps leads to more scattering in the channel and reduces the carrier mobility. The understanding of the defects determining the degradation of proton-induced irradiation will be discussed in the next chapter.

## Chapter V

### Low Frequency $1/f$ Noise Measurement

#### Introduction

Low frequency  $1/f$  noise is measured for AlGaIn/GaN HEMTs over a frequency span of 6 Hz to 390 Hz. In this work, the temperature-dependent noise measurement was taken to provide helpful information on defect energy distribution. As the threshold voltage changes with temperature, the gate voltage is adjusted for a fixed increment from pinch-off voltage so that the noise originates from the gated portion of the channel (will be discussed in the next section). The drain-source bias is maintained at 0.15 V.

#### Gate Bias Dependence of $S_{vd}$

The simplified cross-section of the device is shown in Fig. 5-1. The gate length  $L_G$  is 0.7  $\mu\text{m}$ , while the separation from drain and source are 1  $\mu\text{m}$  and 0.5  $\mu\text{m}$ , respectively. The low frequency noise originates from the channel, both the gated and ungated portion. The resistance of the ungated portion  $R_U$  is approximately constant while the resistance of the gated portion  $R_G$  changes with varies with  $V_G$ , [54] shown as

$$R_G = \frac{L_G V_{th}}{Wq\mu n_{ch}(V_G - V_{th})} \quad (4)$$

where  $\mu$  is the carrier mobility and  $n_{ch}$  is the carrier density.

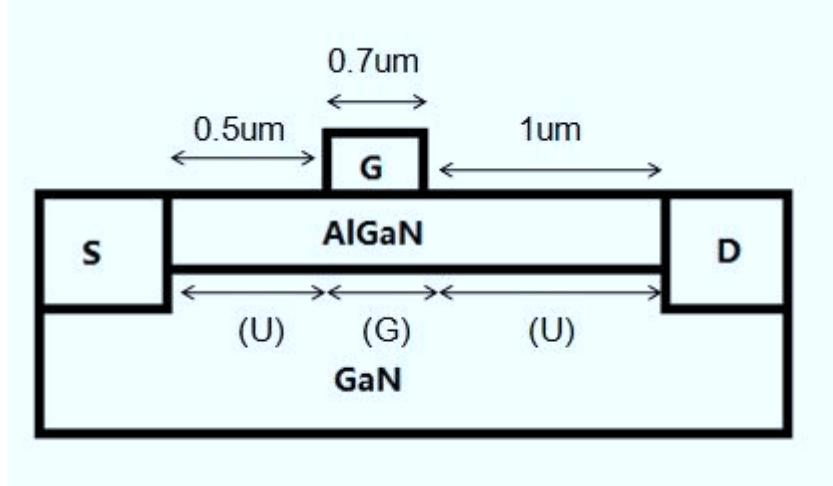
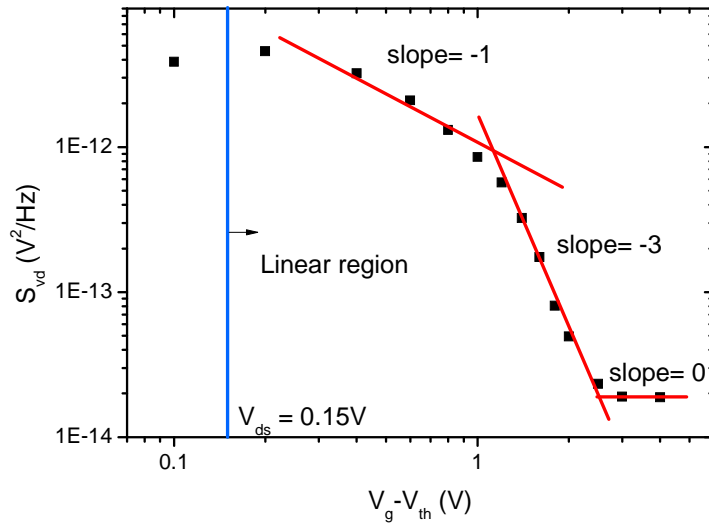
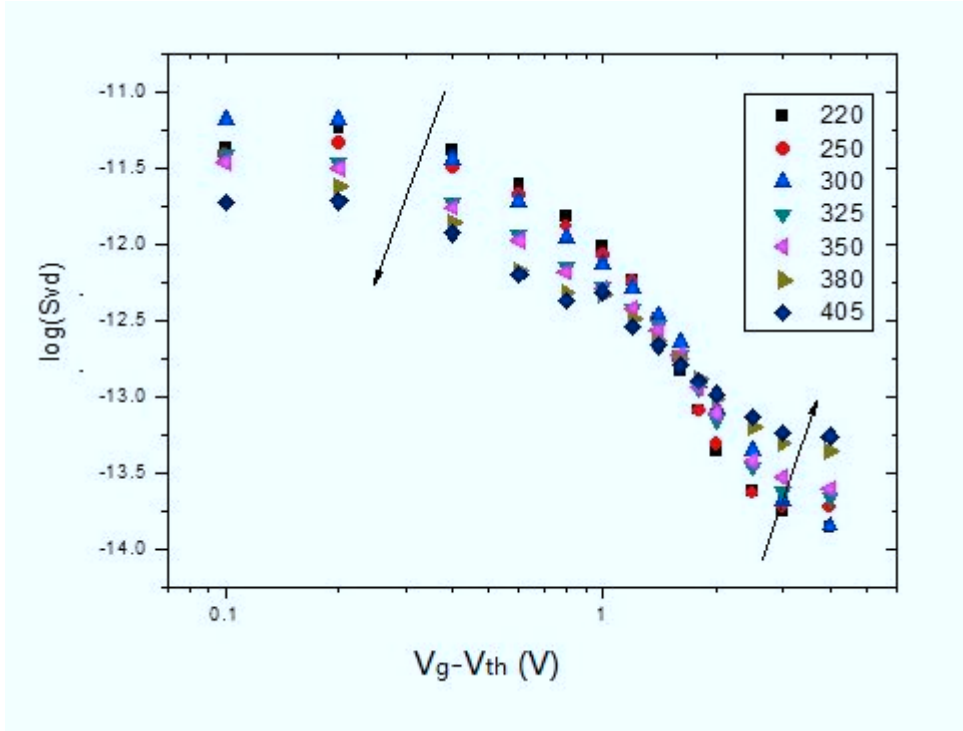


Fig. 5-1 Cross-section of a GaN HEMT, “U” and “G” stands for the ungated and gated portion of the channel.

The HEMT was biased at  $V_{ds} = 0.15$  V in the linear region ( $V_g - V_{th} > 0.15$  V). The power spectrum is shown in Fig. 5-2 (a) as a function of gate voltage. There are three regions observed, with the slope of  $\frac{\log(S_{vd})}{\log(V_g - V_{th})} = -1, -3$  and 0.



(a)



(b)

Fig. 5-2 (a) Gate voltage dependence of excess drain voltage low frequency noise in AlGaIn/GaN HEMTs, at room temperature, (b) Gate voltage dependence at different temperatures.

The change in slopes can be explained from a fixed noise contribution due to  $R_U$  and a noise contribution from the gated portion  $R_G$ , which varies with  $V_G$ . The two contributions are uncorrelated, shown as

$$S_{R_{total}} = S_{R_G} + S_{R_U} \quad (5)$$

For the  $I/f$  noise in a 2DEG, the empirical relation [55] is used, shown as

$$\frac{S_V}{V^2} = \frac{S_I}{I^2} = \frac{S_R}{R^2} = \frac{\alpha}{fN} \quad (6)$$

with  $N$  is the number of free charge carriers in the channel. Hence, the bias dependence of the two contributions can be expressed as

$$S_{R_G} = \frac{\alpha R_G^2}{fN_G} \propto V_G^{-3} \quad (7)$$

$$S_{R_U} = \frac{\alpha R_U^2}{fN_U} \propto V_G^0 \quad (8)$$

where  $N_G$  is the number of carrier under the gate, which is proportional to gate bias while  $N_U$  is the number of carriers in the ungated channel.

When the gate is biased very close to the threshold voltage, there are only a few electrons in the channel. In this condition, the resistance from the gated portion is larger than that of the ungated portion ( $R_G > R_U$ ). When the noise is dominated by the gated portion ( $S_{R_G} > S_{R_U}$ ), the noise is found as

$$\frac{S_V}{V^2} = \frac{S_R}{R^2} = \frac{S_{R_G}}{R_G^2} = \frac{\alpha}{fN_G} \propto V_G^{-1}. \quad (9)$$

When the gate bias increases, there are sufficiently high density of electrons in the channel while the resistance of the gated portion decreases ( $R_G < R_U$ ). The noise originating from the gated portion is then described as

$$\frac{S_V}{V^2} = \frac{S_R}{R^2} = \frac{S_{R_G}}{R_U^2} = \frac{\alpha}{fN_G} \frac{R_G^2}{R_U^2} \propto V_G^{-3}. \quad (10)$$

At even larger bias, both the resistance and the noise are dominated by the parasitic series resistance ( $R_G < R_U$ ,  $S_{R_G} < S_{R_U}$ ). In this condition, the noise is not dependent on the gate bias:

$$\frac{S_V}{V^2} = \frac{S_R}{R^2} = \frac{S_{R_U}}{R_U^2} = \frac{\alpha}{fN_U} \propto V_G^0. \quad (11)$$

In the following measurement, the device was biased in the region of slope = -3, which ensures the noise originates from the channel with an approximately constant

total resistance ( $R_{total} \approx R_U$ ).

Fig. 5-2(b) shows the gate voltage dependence at different temperatures, from 200K to 400K. The changes in noise level indicate the changes in defect distribution, which will be discussed later. As temperature get higher, the range with slope = -3 became flatter. This is because at higher temperatures, the resistance in the channel becomes larger due to more scatterings so that the resistance from the gated portion cannot be neglected.

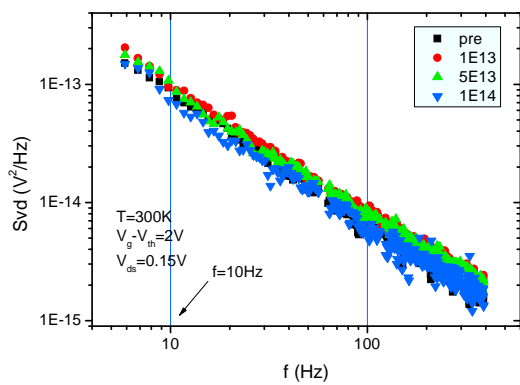
### **Noise Spectrum of AlGaIn/GaN HEMTs**

Low frequency  $1/f$  noise can provide helpful information about the nature of the defects that limit the reliability of semiconductor devices. The trap density is associated with noise level and the bias and temperature condition of the measurement, shown as

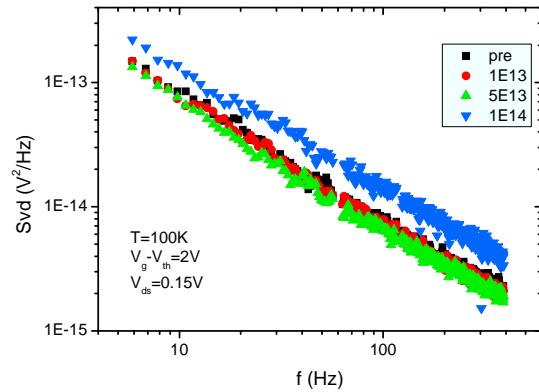
$$N_{trap} \propto S_V f^\gamma (V_g - V_{th})^2 (V_d)^{-2} T^{-1}, \gamma = -\frac{\ln S_V}{\ln f}. \quad (12)$$

If the bias condition and temperature are fixed, the trap density is proportional to the noise level and the frequency exponent. Fig. 5-3 shows the noise level before and after irradiation, at different temperatures. At room temperature 300 K, the noise level at 10 Hz decreased with increasing fluence (Fig. 5-3 (a)); at 100 K, it didn't change much at small fluences, and increased rapidly after a fluence of  $10^{14}/\text{cm}^2$  (Fig 5-3(b)); at 400 K, the 10 Hz noise decreased a little after irradiation and stayed almost

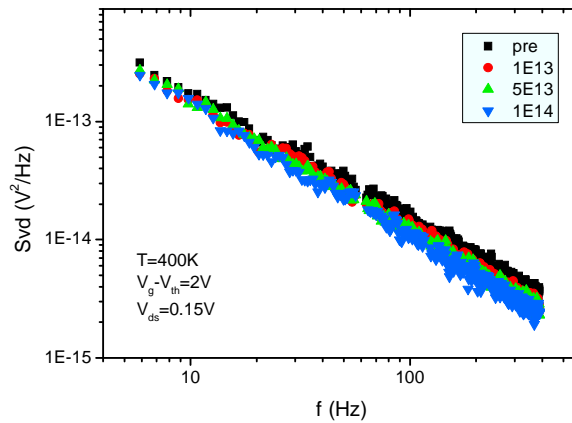
constant.



(a)



(b)



(c)

Fig. 5-3 Noise vs. frequency before and after proton irradiation at different temperatures: (a) 300 K, (b) 100 K and (c) 400 K.

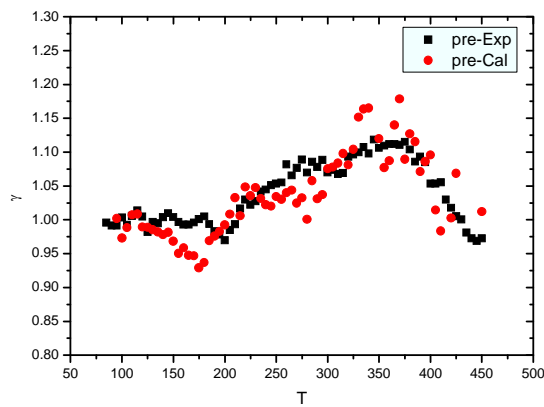
At different temperatures, the noise levels increase or decrease after irradiation. This suggests that the measurement at a fixed temperature may mislead the change in defect formation and a noise measurement over a large temperature range can avoid getting wrong conclusions. The temperature-dependent noise measurement is performed from 85 K to 450 K, at a fixed bias condition of  $V_{ds}$  and  $V_g - V_{th}$ . Fig. 5-4



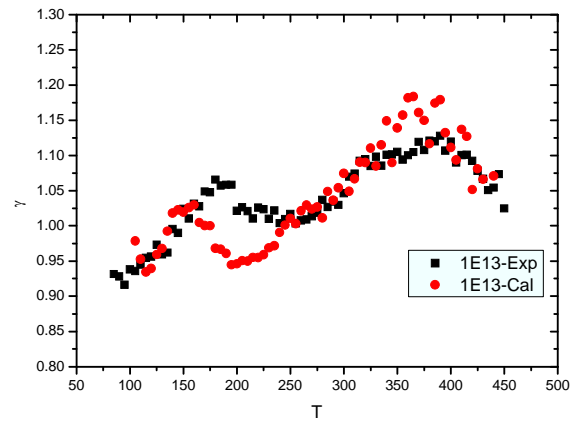
shows the frequency exponent  $\gamma$  as function of temperature T. The Dutta and Horn model [48] describes the frequency and temperature dependence of noise via

$$\gamma(\omega, T) = 1 - \frac{1}{\ln(\omega\tau_0)} \left( \frac{\partial \ln S(\omega, T)}{\partial \ln T} - 1 \right), \quad (13)$$

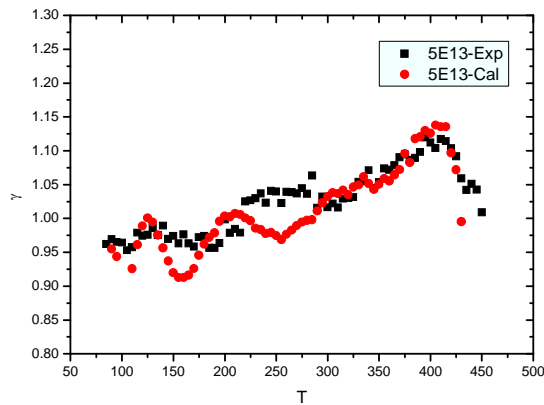
where  $\tau_0$  is the attempt-to-escape frequency of the defect.



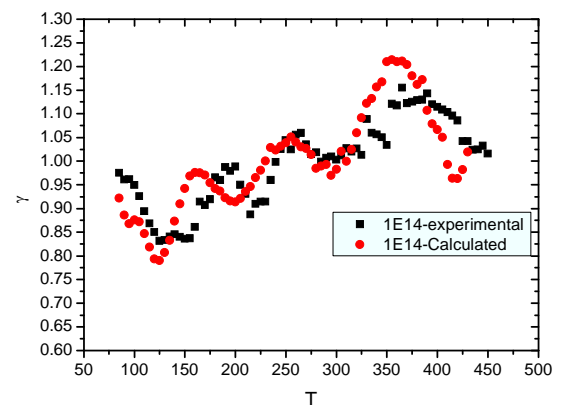
(a)



(b)



(c)



(d)

Fig. 5-4 Frequency exponent of noise power spectral density as a function of temperature. The experimental data fits the Dutta-Horn model closely.

The calculated and experimental values of  $\gamma$  match closely at different proton

fluences, indicating that the noise is originated from the thermal transition between two metastable charge states of a defect. The activation barrier  $E_0$  is proportional to the temperature via

$$E_0 = -kT \ln(\omega\tau_0), \quad (14)$$

where  $k$  is the Boltzmann constant,  $\omega = 2\pi f$  and  $\tau_0$  is the characteristic time for the defect, which is  $3 \times 10^{-14}$  s in this work. The value of  $\gamma$  increases with increasing temperature, suggesting that for defects in the AlGaIn, charge exchange between AlGaIn and GaN occurs via a thermally activated process instead of tunneling. [56]

As the experimental data follow the Dutta-Horn model well, the activation energy distribution of defects can be estimated via

$$D(E_0) \propto \frac{\omega}{kT} S(\omega, T), \quad (15)$$

which is plotted as a function of  $T$  in Fig. 5-5. The top X axis is the activation energy calculated from the bottom axis of temperature. The noise spectrum before irradiation (black) exhibits two peaks located at  $\sim 0.2$  eV and 0.9 eV. After a small fluence of irradiation, the peak at 0.9 eV decreased while the 0.2 eV increased. Meanwhile a small increase at  $\sim 0.6$  eV was observed. After a fluence of  $1 \times 10^{14}$  protons/cm<sup>2</sup>, this new peak decreased largely while the 0.2 eV peak increased significantly. The changes in peaks at different fluences directly show how the defect distribution changed after irradiation.

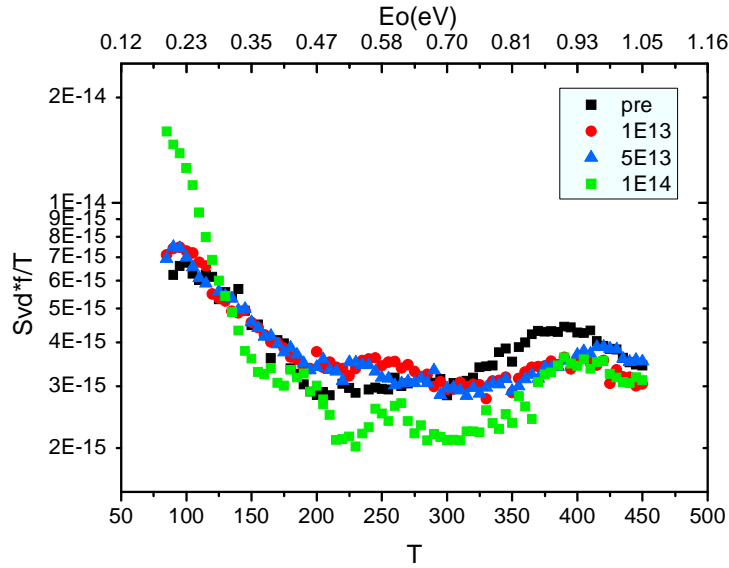


Fig. 5-5 The noise spectrum power density, equivalent to the noise activation energy distribution, as a function of  $T$ , at different proton irradiation fluences.

The 0.2 eV peak often observed in AlGaIn/GaN noise is most likely due to an oxygen DX center, i.e., an  $O_N$ . [49][57] The energy barrier for thermal excitation between  $O^{-1/0}$  charge states is  $\sim 0.25$  eV. Extensive calculations show that the 0.9 eV and 0.6 eV peaks are associated with hydrogenated oxygen DX centers; that is,  $O_N\text{-H}$  defects. The calculations show that  $0^{-1}$  charge transition levels of the  $O_N\text{-H}$  defect complexes are 0.8 and 0.6 eV below the AlGaIn conduction band minimum for configurations I and II in Fig. 5-6, respectively. During proton irradiation, the H atom can be removed from the  $O_N\text{-H}$  (e.g., via interaction with transporting holes) with a low energy barrier, as illustrated in Fig. 5-6. Hence, both the decrease in 0.9 eV defect density and the increase in 0.2 eV defect density can be related to hydrogen removal from the  $O_N\text{-H}$  complex (Fig. 5-6 (a)), reducing the  $O_N\text{-H}$  density and increasing the  $O_N$  density. The small peak near 0.6 eV is associated with an intermediate

configuration of the  $O_N$ -H complex, shown as configuration II in Fig. 5(a).

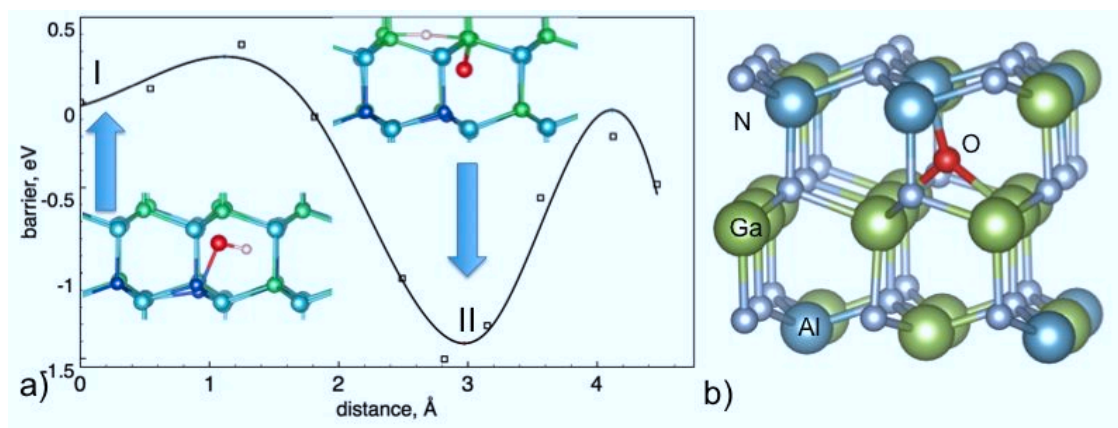


Fig. 5-6 (a) Energy barriers and defect configurations (I) and (II) of  $O_N$ -H (smaller light atom) and (b)  $O_N$  configuration.

The low temperature peak increased rapidly after  $1 \times 10^{14}$  protons/cm<sup>2</sup>, which suggests that there can be other processes happened. People using 2 MeV protons observed a defect labeled as ER1, with an energy level  $\sim 0.13$  eV below the conduction band is a possible candidate in this case. [58][59]

### Conclusions

In this chapter, via 1/f noise measurement, the changes in defect distribution after irradiation is studied. The defect energy spectrum of AlGaN/GaN HEMTs show peaks at 0.2 eV and 0.9 eV before irradiation and by removing H atoms from the hydrogenated  $O_N$  defect complex during the irradiation, 0.9 eV peak decreased while 0.2 eV increased. A new peak at 0.6 eV appeared and decreased, showing the

intermediate state of defect reconfiguration.

## Chapter VI

### Hot Carrier Effects on AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs

#### Introduction

Degradation induced by hot carriers, such as the reduction of transconductance and shift in threshold voltage, is an impediment for Ga<sub>N</sub> HEMTs in high power and high frequency applications. [60][61] Hydrogen, as a component of most gases and liquids, diffuses rapidly into Ga<sub>N</sub> during fabrication processes, such as growth, annealing and etching. [62] The interactions between hydrogen and defects lead to hydrogenation of defects and play an important role in Ga<sub>N</sub> reliability issues.[63][64][65]

In this chapter, the hot-carrier-induced degradation in AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs is reported. The HEMTs were subjected to room-temperature electrical stress and the noise spectrum before and after stress were taken to monitor the changes in defect distribution. A negative shift in threshold voltage is observed, with a peak transconductance degradation of 13%.

#### Experiment Settings

The AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs are stressed at a drain-source bias of 10V, with the gate

bias very close to the pinch-off voltage, providing a strong field at the gate-drain access region that enhances hot electron effects. The devices were stressed for a sufficiently long time until all the changes were saturated.

### DC Measurements and Noise Spectrum Analysis

Fig. 6-1 shows a negative shift in threshold voltage of 45 mV, which indicates more positive charge trapping. The threshold voltage shift direction was different from that of proton irradiation, implying different defect dominated during the experiment. The peak transconductance degraded about 13% after stress, which is shown in Fig. 6-2. More traps were generated and the mobility of carriers decreased due to more scattering.

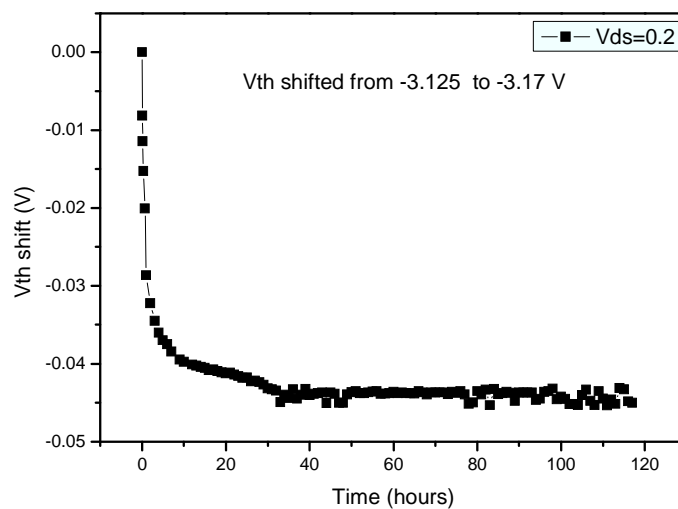


Fig. 6-1 Threshold voltage shift as a function of time.

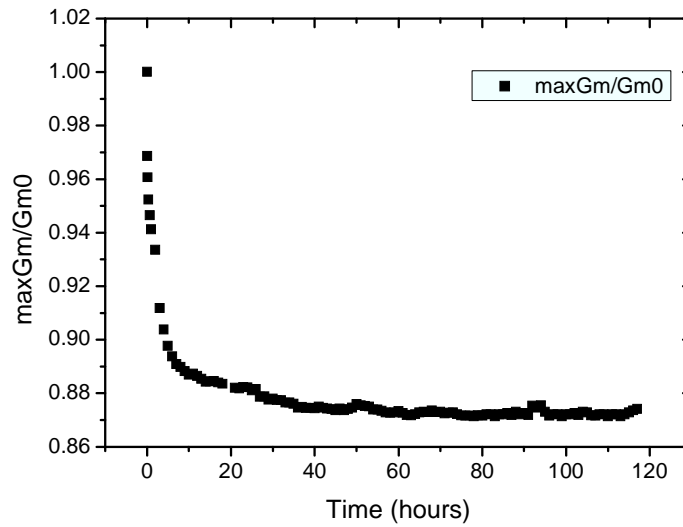


Fig. 6-2 Normalized peak transconductance degradation as a function of time.

The noise spectrum before and after stress is shown in Fig. 6-3, using the same measurement techniques in Chapter V. Before electrical stress, there are two peaks at 0.2 eV and 0.9 eV, showing the same features as before proton irradiation. After hot carrier stress, the changes in three peaks agree with that after proton irradiation: the 0.9 eV peak decreased a little with an increase in 0.2 eV; at the position of 0.6 eV, the noise level decreased. As hot electrons can dehydrogenate point defects via single scattering events or by multiple vibrational excitations, the hot-carrier-induced noise spectrum change confirmed that during the proton irradiation, H atoms are removed from  $O_N$ -H complex and play an important role in proton-induced degradation.

The threshold voltage shift direction is opposite after hot carrier stress and proton irradiation, indicating different dominant defects in the devices. Under proton exposure, the defects can be generated over a larger space, (e.g., in the AlGaIn, at the interface and in the channel) as proton bombardment covered the total area of the



device; while hot electrons are generated only at the gate-drain access region. It is reasonable that different defects were generated under different mechanisms. The temperature dependent noise spectrum only observed the distribution of defects with activation energy from 0.16 eV to 1.05 eV and limits the observation of higher energy levels.

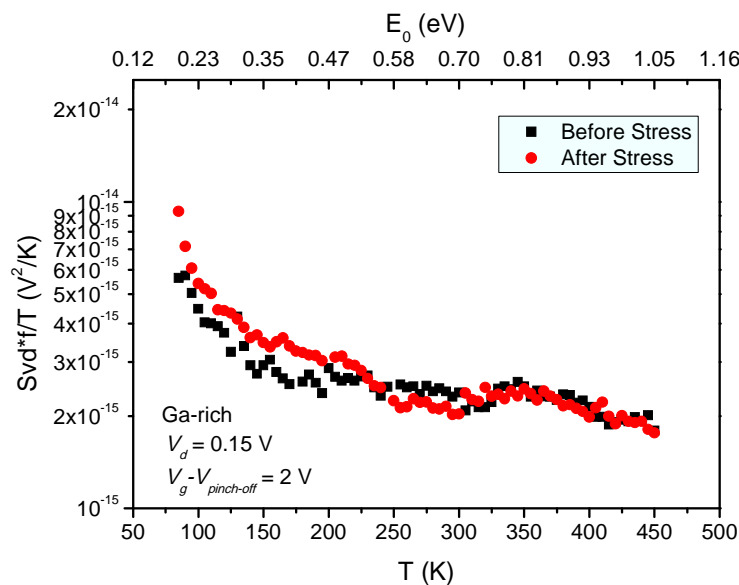


Fig. 6-3 Noise spectrum before and after hot carrier stress.

### Conclusions

Negative shift in pinch-off voltage and transconductance reduction is observed after hot carrier stress. The nature of the defects determining the degradation induced by hot electrons is different from that of proton irradiation. However, the noise spectrum exhibits the same features as that after proton irradiation, indicating the dehydrogenation of  $O_N-H$  defects is a major process during proton bombardment.

## Chapter VII

### Summary and Conclusions

In this work, we have performed radiation exposure and hot carrier stress on AlGaIn/GaN HEMTs. The device exhibited excellent radiation tolerance to 10 keV X-ray irradiation as there is no oxide layer in the device structure. Larger shifts in DC characteristics were observed after 1.8 MeV proton irradiation and electrical stress. We employed low frequency  $1/f$  noise as a diagnostic tool to understand the nature of the defects that dominate the degradation. Density function theory calculations show the formation energy for the defect might be responsible for the degradation. The techniques used in identification of defects are not limited in GaN-based systems, and can be used in any semiconductor material.

When subjected to 1.8 MeV protons, a positive shift in pinch-off voltage is observed, with degradation a peak transconductance due to the generation of acceptor-like traps. The  $1/f$  noise changes after irradiation at different temperatures, indicating the possible changes in defect distribution. We showed the gate voltage dependence of the noise, and found a bias condition that focused the noise from the gated region with almost constant total resistance. We also showed that the experimental noise data fits the Dutta-Horn model well, which enables us to translate the noise change to thermal transition between two charge states of the defect. Before irradiation, the device originally shows two peaks at 0.2 eV and 0.9 eV. After

irradiation, the 0.9 eV peak decreased while the 0.2 eV peak increased. DFT calculations shows that this change is related to H atoms removed from an  $O_N$ -H defect, and a new peak increased and then decreased after irradiation at 0.6 eV was found as an intermediate configuration of the defect.

When the devices are stressed at high electric field, hot carriers are generated. Unlike protons, hot electrons with much smaller energy do not generate defects but interact with pre-existing defects, like dehydrogenation of defects. The noise spectra before and after stress show similar features as that of proton irradiation, confirming that protons dehydrogenate  $O_N$ -H defects during the irradiation. The threshold voltage shift is negative, which is opposite compared with that after proton exposure, due to different defects determining the degradation. The defect is not detected via the temperature dependent noise measurement, owing to temperature limitations of the device packaging.

In summary, we have used radiation and DC stress to understand the degradations in AlGaIn/GaN HEMTs. The low frequency  $1/f$  noise and density functional theory calculations helped to identify the defects that limit the performance of the devices.

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